

AD-A067 221 VIRGINIA UNIV CHARLOTTESVILLE DEPT OF MECHANICAL AND--ETC F/G 13/9
HIGH SPEED ROTOR BALANCING.(U)
DEC 78 W D PILKEY

UNCLASSIFIED

UVA/525088/MAE78/102

ARO-15080.7-E

DAA629-78-G-0019
NL

| OF |

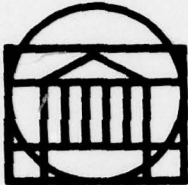
AD
A067221



END
DATE
FILMED
6-79
DDC

ADAO 67221

DDC FILE COPY



LEVEL

RESEARCH LABORATORIES FOR THE ENGINEERING SCIENCES

SCHOOL OF ENGINEERING AND APPLIED SCIENCE

UNIVERSITY OF VIRGINIA

Charlottesville, Virginia 22901

15 DAAG 29-78-G-0019

Final Report

6

HIGH SPEED ROTOR BALANCING

Submitted to:

U.S. Army Research Office
P.O. Box 12211
Research Triangle Park
North Carolina 27709

Attn: DRXRO-PP-L-15080-E
Richard O. Ulsh, Chief
Information Processing Office

Submitted by:

10

Walter D. Pilkey
Professor

9 Final rept. 22 Oct 77 - 30 Nov 78

APPROVED FOR PUBLIC RELEASE:
DISTRIBUTION UNLIMITED

12 14p

Report No. UVA/525088/MAE78/102

11 December 1978

410 696

79 04 09 024

18 ARO 15080.7-E
12

DDC
RECEIVED
APR 10 1979
C

RESEARCH LABORATORIES FOR THE ENGINEERING SCIENCES

Members of the faculty who teach at the undergraduate and graduate levels and a number of professional engineers and scientists whose primary activity is research generate and conduct the investigations that make up the school's research program. The School of Engineering and Applied Science of the University of Virginia believes that research goes hand in hand with teaching. Early in the development of its graduate training program, the School recognized that men and women engaged in research should be as free as possible of the administrative duties involved in sponsored research. In 1959, therefore, the Research Laboratories for the Engineering Sciences (RLES) was established and assigned the administrative responsibility for such research within the School.

The director of RLES—himself a faculty member and researcher—maintains familiarity with the support requirements of the research under way. He is aided by an Academic Advisory Committee made up of a faculty representative from each academic department of the School. This Committee serves to inform RLES of the needs and perspectives of the research program.

In addition to administrative support, RLES is charged with providing certain technical assistance. Because it is not practical for each department to become self-sufficient in all phases of the supporting technology essential to present-day research, RLES makes services available through the following support groups: Machine Shop, Instrumentation, Facilities Services, Publications (including photographic facilities), and Computer Terminal Maintenance.

HIGH SPEED ROTOR BALANCING

FINAL REPORT

WALTER D. PILKEY

1978

U. S. ARMY RESEARCH OFFICE

GRANT NO. DAAG29 78 G 0019

UNIVERSITY OF VIRGINIA

APPROVED FOR PUBLIC RELEASE;
DISTRIBUTION UNLIMITED.

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ME-5-25088-102-70	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) HIGH SPEED ROTOR BALANCING		5. TYPE OF REPORT & PERIOD COVERED Final
7. AUTHOR(s) Walter D. Pilkey		6. PERFORMING ORG. REPORT NUMBER DAAG29 78 G 0019
9. PERFORMING ORGANIZATION NAME AND ADDRESS		8. CONTRACT OR GRANT NUMBER(s) ↓
11. CONTROLLING OFFICE NAME AND ADDRESS U.S. Army Research Office Post office Box 12211 Research Triangle Park NC 27709		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE 1978
		13. NUMBER OF PAGES 9
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE NA
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) NA		
18. SUPPLEMENTARY NOTES The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Rotating Shaft Balancing Rotor Dynamics Dynamics		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report summarizes the accomplishments of the final year of a study exploring new methods for balancing, analyzing and designing flexible rotating shafts. A technique for identifying rotor bearing parameters is proposed. Then a quadratic programming formulation is presented for influence coefficient balancing with constraints. Finally, a method is developed for determining the optimal axial location of balancing planes.		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE
S/N 0102-LF-014-6601

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

PROBLEM STATEMENT AND ACCOMPLISHMENTS

The goal of the program is to explore new techniques for balancing, analyzing, and designing rotating shafts. This study began with the assumptions that the balancing problem is rightfully classified as an identification/optimization problem and that modern computational techniques hold great promise in aiding in the solution of the problem. Throughout the study emphasis is given to computational optimization formulations.

The achievements of the final year of this study, which was performed during the period 21 October 1977 - 30 November 1978, can be grouped into three categories:

- Estimation of Parameters in a Linear Rotor-Bearing System Model
- The Determination of Rotor Balance Weights by Quadratic Programming Models
- Study of the Sensitivity of the Balanced-Rotor Residual Deflections to Deletions of Balancing Weights

These efforts are summarized below.

I. The Estimation of Parameters in a Linear Rotor-Bearing System Model

For a system of ordinary, linear differential equations with constant coefficients which models a rotor-bearing system, the problem of estimating viscous damping constants and other parameters which appear in the model is approached from an optimization standpoint. The magnitudes of the constants are adjusted to give the best agreement between some measured values of the system properties and the values computed from the model. An estimation method is developed whereby a steepest descent or creeping random search optimization algorithm is applied to the linear algebraic equations which govern the rotor's steady state response. The optimization is

conducted. The optimization is conducted at a single frequency and it requires that at least as many displacement measurements be obtained as there are unknown parameters to be estimated. Because the actual response characteristics of the rotor bearings are known to be nonlinear, the confinement of the optimization to a single frequency should result in a linear model which is useful in some range about that frequency. Of course, if the linear model is to apply over a wide range of frequencies, the optimization can be performed using measurements taken at a number of rotor speeds.

II. The Determination of Rotor Balance Weights by Quadratic Programming Models

In the influence coefficient method of balancing, the rotor response is expressed as a linear function of applied unbalance weights. Let (x,y,z) represent a system of coordinates rotating at the rotor spin speed about the z -axis, which is parallel to the undeformed shaft axis. In an isotropic system, the orbit of the geometric centroid of the shaft cross section can be considered to be circular as it undergoes synchronous whirl due to unbalance inertia forces.

Let $\overline{W}_X, \overline{W}_Y$ represent the components of deflections at various locations along the rotor axis. Let $\overline{U}_X, \overline{U}_Y$ represent components of masses applied to the rotor. Let $[A_X], [A_Y]$ be matrices of influence coefficients relating the in-phase and out-of-phase components of deflection to the applied unbalances ($[A_X]$ and $[A_Y]$ are independent of the orientation of the coordinates).

$$\overline{W} = \overline{W}_X + j \overline{W}_Y \quad (j = \sqrt{-1})$$

$$\overline{U} = \overline{U}_X + j \overline{U}_Y$$

$$[A] = [A_X] + j [A_Y]$$

$$\overline{W} = [A] \overline{U}$$

ACT 50-1-6	NTIS	White Section	<input type="checkbox"/>
DOC	UNANNOUNCED	Blue Section	<input type="checkbox"/>
	JUSTIFICATION		<input type="checkbox"/>
by	DATE	TIME	INITIALS

A

Let \overline{WM} be a vector of displacements measured along the rotor which are caused by intrinsic (not applied) mass unbalance. A typical rotor balancing procedure computes correction weights by minimizing the sum of the squares of the residual rotor deflection:

$$E = (\overline{WM} + \overline{W})^T (\overline{WM} + \overline{W}) = (\overline{WM} + [A]\overline{U})^T (\overline{WM} + [A]\overline{U})$$

In the case in which the elements of \overline{U} are unconstrained, the balance weights are obtained by solving the set of linear equations $\text{GRAD}(E) = \overline{0}$, in which the gradient components are derivatives with respect to the elements of \overline{U} . Often, the balance weights computed by this method are too large to conveniently apply to the rotor. To overcome this problem, the expression for E can be minimized subject to upper bounds on the components of \overline{UX} and \overline{UY} . Let \overline{X} denote a vector the components of which are sets of pairs of real number (UX, UY) for each balance plane. Carrying out the multiplications in the expression for E results in:

$$E = W_0 + \overline{C}^T \overline{X} + \overline{X}^T [D] \overline{X}$$

W_0 is the sum of the squares of the measured deflections.

\overline{C} is the cost vector (a function of \overline{WM} and $[A]$).

$[D]$ is the quadratic matrix which is assumed to be positive definite ($[D]$ is a function of $[A]$).

Let \overline{UM} be a vector of the upper and lower bounds on the elements of \overline{X} .

$$- \overline{UM} \leq \overline{X} \leq \overline{UM}$$

By introducing a shift of coordinates, these constraints can be converted to the form $\overline{0} \leq \overline{X}' \leq \overline{UM} + \overline{UM}$ in which $\overline{X}' = \overline{X} + \overline{UM}$.

In this study, a quadratic programming routine was employed to demonstrate the usefulness of the quadratic programming algorithm to rotor balancing.

III The Study of the Sensitivity of the Balanced-Rotor Residual Deflections to Deletions of Balancing Weights

The third study deals with the problem of estimating which of N possible balance places can be deleted with the smallest increase in the rotor residual deflection. Because this process will involve the simultaneous, finite change of the variables of a quadratic function, a computationally attractive exact method of finding the correct answer does not appear to be possible. Suppose that the optimal choice of n of N possible planes ($n < N$) is sought; then, there will be $\frac{N!}{n!(N-n)!}$ possible choices. As N increases, an exhaustive search rapidly becomes impractical (e.g. for $N=20$, there are 184,756 possible choices of 10 planes). A random search algorithm could be a feasible approach; for example, the probability of finding a solution in the best 1% of all solutions is better than 99% with a random sample of 500 trials. However, running even 500 problems is a fairly unattractive alternative.

Because only n -plane solutions which do not too greatly increase the rotor residual deflection from the N -plane level are of interest, a region near the N -plane optimum may exist where variable interactions can be neglected in estimating the effects of balance plane deletions. Any technique which attempts to consider the interactions of deleted balance planes would entail examination of all or a great number of the $N!/(N-n)!n!$ possibilities. By considering only independent effects, a small fraction of the great number of possibilities can be segregated for exact solution.

To estimate the effects of balance plane deletions, two studies were conducted. In the first, the unconstrained solution with N -planes was obtained; then N additional problems were solved in which the upper bounds

on one of the N-planes was reduced either to zero or to a very small value. From the change in the objective function and the value of the Lagrange multiplier for each deleted variable, the most insensitive balance plane can be estimated. These estimated selections are then compared with actual n-plane solutions determined by exhaustive or random searches.

In the second study, the constraint limits were allowed to approach zero simultaneously, and the order in which constraints become active, the change in the objective function as constraints decreased, and the changes in the Lagrange multipliers were studied. This information was used to estimate balance plane sensitivity, as in the first study. These results indicate that independent effects can be used to estimate the sensitivity of the rotor balance level to plane deletions.

LIST OF PUBLICATIONS (1974-1978)

1. "A Linear Programming Approach for Balancing Flexible Rotors", R. M. Little and W. D. Pilkey, The Journal of Engineering for Industry, Vol. 94, 1976.
2. "Constrained Balancing Techniques for Flexible Rotors", W. D. Pilkey and J. T. Bailey, The Journal of Engineering for Industry, 1978.
3. "Identification of Shock and Vibration Forces", W. D. Pilkey and A. J. Kalinowski, in ASME Monograph, Identification of Vibration Structures, 1972.
4. "A Worst Balance Analysis for Rotating Shafts," W. D. Pilkey and J. T. Bailey, J. of Sound and Vibration, 1974.
5. "Response Bounds for Structures with Incompletely Prescribed Loadings," W. D. Pilkey and A. J. Kalinowski, Shock and Vibration Bulletin, Vol. 43, 1972.
6. "Efficient Optimal Design of Suspension Systems for Rotating Shafts," W. D. Pilkey, B. P. Wang, and D. Vannoy, The Journal of Engineering for Industry, Vol. 98, 1976.
7. "Structural Design for Incompletely Prescribed Loading," W. D. Pilkey and A. J. Kalinowski, Engineering Mechanics Journal, ASCE, 1975.
8. "Limiting Performance, Identification, and Optimal Design of Vibromechanisms," Proc. of 3rd International Conference on Vibromechanisms, 1974.
9. "Rotating Machinery, A Review of Computational Capabilities," H. Shapiro, G. Horner, and W. D. Pilkey, in Shock and Vibration Computer Programs, SVIC, 1975.
10. "Rotating Shafts", W. D. Pilkey and P. Y. Chang, in Modern Formulas for Statics and Dynamics, McGraw Hill, 1978.
11. "Transient Response of a Rotor in Damped Bearings," J. Strenkowski and W. D. Pilkey, ASME Paper No. 77-DET-21, J. of Engineering for Industry, 1978
12. "The Riccati Transfer Matrix Method," G. C. Horner and W. D. Pilkey ASME Paper No. 77-DET-32, J. of Engineering for Industry, 1978.
13. "Complex Infinite Beams on an Elastic Foundation," P. Y. Chang, D. Hsu, and W. Pilkey J. of the Structural Division, ASCE, Vol. 103, No. ST11, November, 2277-2282, 1977.

14. "The Estimation of Parameters in a Linear Rotor-Bearing System Model", E. Woerner and W. D. Pilkey, in booklet Dynamics of Rotor-Bearing Systems, ASME, 1978.

Other papers are being considered for publication.

PARTICIPATING PERSONNEL (During Final Year)

W. D. Pilkey, Principal Investigator

C. Thasanatorn, Received Ph.D. degree

F.H. Chu, Received Ph.D. degree

M. Taylor, Received Ph.D. degree

E. Woomer, Ph.D. Candidate

DISTRIBUTIONNo. of Copies

60	U. S. Army Research Office - Research Triangle Park
5	Principal Investigator (Pilkey)
1	Department Files (S. Fletcher)
1	C. B. Thomas, University of Virginia
3	RLES, University of Virginia Files

UNIVERSITY OF VIRGINIA

School of Engineering and Applied Science

The University of Virginia's School of Engineering and Applied Science has an undergraduate enrollment of approximately 1,300 students with a graduate enrollment of approximately 500. There are 125 faculty members, a majority of whom conduct research in addition to teaching.

Research is an integral part of the educational program and interests parallel academic specialties. These range from the classical engineering departments of Chemical, Civil, Electrical, and Mechanical and Aerospace to departments of Biomedical Engineering, Engineering Science and Systems, Materials Science, Nuclear Engineering and Engineering Physics, and Applied Mathematics and Computer Science. In addition to these departments, there are interdepartmental groups in the areas of Automatic Controls and Applied Mechanics. All departments offer the doctorate; the Biomedical and Materials Science Departments grant only graduate degrees.

The School of Engineering and Applied Science is an integral part of the University (approximately 1,530 full-time faculty with a total enrollment of about 16,000 full-time students), which also has professional schools of Architecture, Law, Medicine, Commerce, and Business Administration. In addition, the College of Arts and Sciences houses departments of Mathematics, Physics, Chemistry and others relevant to the engineering research program. This University community provides opportunities for interdisciplinary work in pursuit of the basic goals of education, research, and public service.